

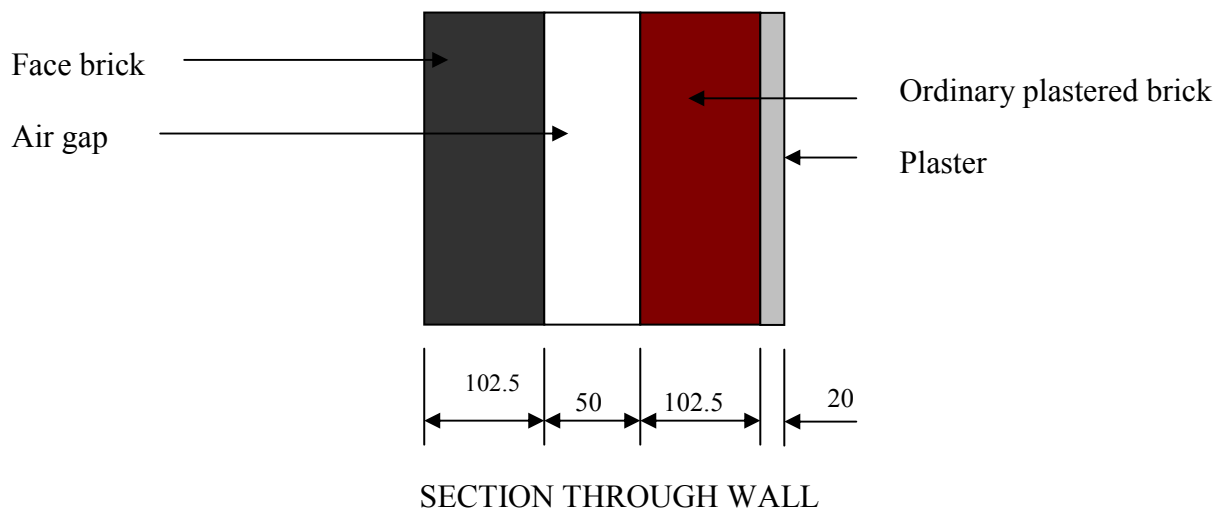
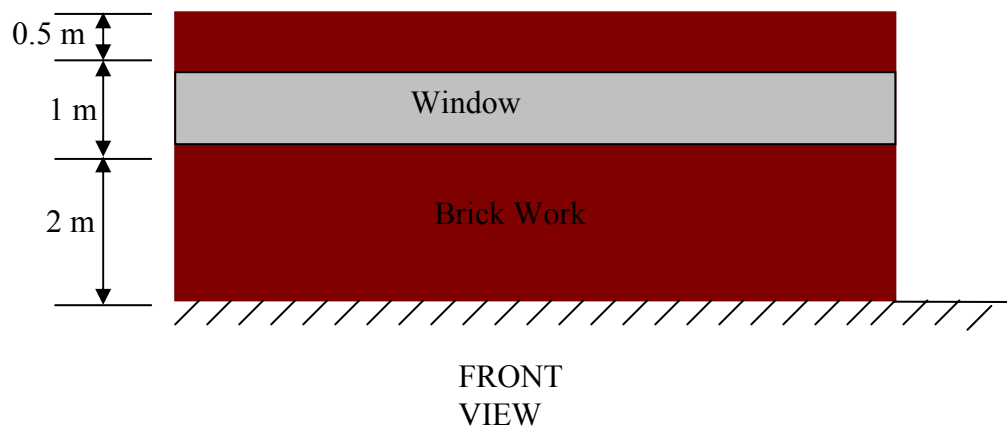
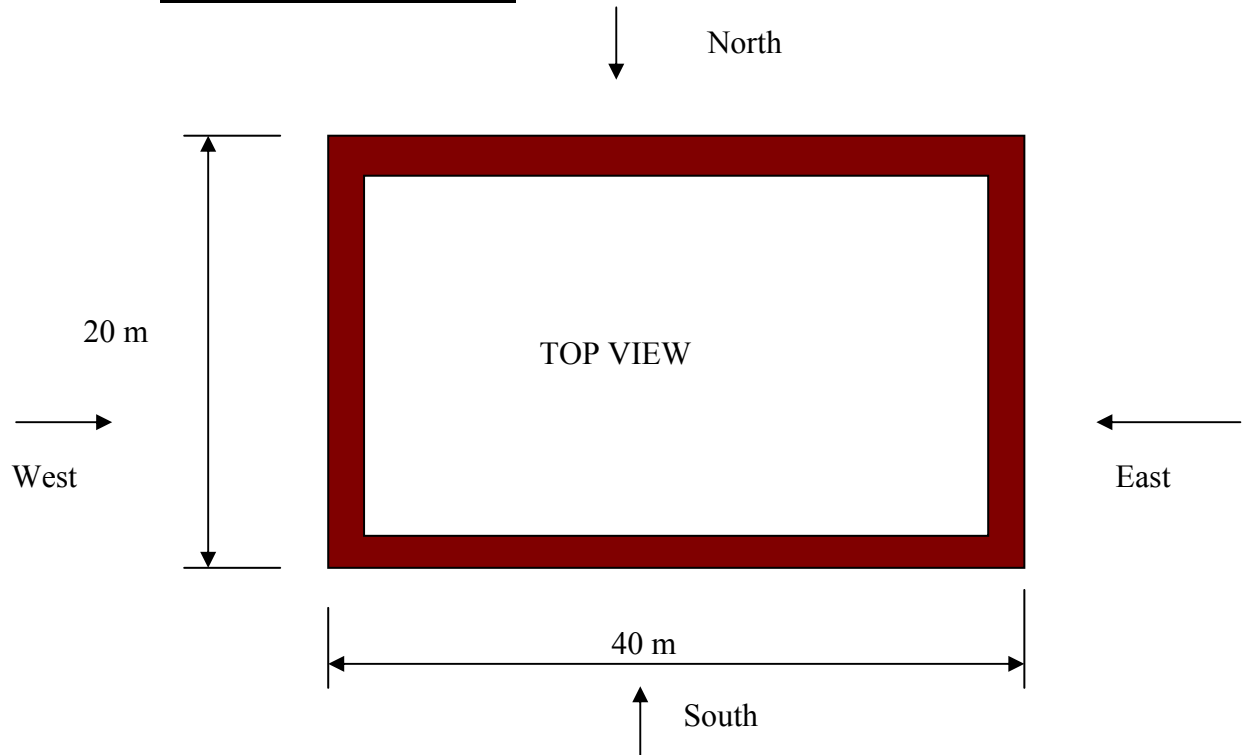
**NISHAL MANILALL**

**STUDENT NO : 14427052**

**AIR CONDITIONING AND REFRIGERATION**

**ASSIGNMENT 6 : HEAT LOAD CALCULATIONS II**

# 1. SKETCH OF BUILDING



## **JANUARY DESIGN CONDITIONS**

1. Design room temperature = 24 deg. C
2. Mass of brickwork = density x thickness  
 =  $1830 \times 0.205$  ....0.205 m is two course brick.  
 =  $375.15 \text{ kg/m}^2$
3. Mass of plaster = density x thickness  
 =  $1100 \times 0.02$   
 =  $22 \text{ kg/m}^2$
4. Total mass per unit area for the walls :  
 =  $397.15 \text{ kg/m}^2$  ~  $400 \text{ kg/m}^2$

### Heat gain through Walls

By interpolating from table 21, the following result was achieved for the equivalent temperature difference

EQUIVALENT TEMPERATURE DIFFERENCE - for $400 \text{ kg/m}^2$											
Sun Time	8	9	10	11	12	1	2	3	4	5	6
Exposure											
North	1.65	1.95	2.2	5	6.65	10	12.25	13.35	13.9	13.6	12.75
East	3.9	10.3	14.45	16.35	17.5	14.45	12.8	11.35	10.55	10.25	10
West	3.9	3.9	3.9	4.45	5	6.1	7.25	10.3	12.8	16.4	18.85
South(shade)	1.1	1.4	1.65	1.95	2.2	3.35	4.45	5.3	6.1	6.65	6.95

### Correction for indoor/outdoor temp. difference and the daily range

Outdoor temperature (Cape town at 3pm) - Room design temperature =  $32.2 - 24 = \underline{\underline{8.2^\circ\text{C}}}$ .  
 January daily range =  $32.2 - 22.2 = 10^\circ\text{C}$ , the correction factor as  $-1.8^\circ\text{C}$ .

X

[illegible]

The corrected table is :

[illegible]

### Correction for Lattitude and Wall colour

From Table 5 - Peak Solar Heat Gains:

Cape Town – Latitude – 33°55'; Longitude – 18°27' - Reference attached

Solar Peak Gains through reference glass - JANUARY				
	sigma_M	sigma_S		
North	230	152		
East	550	550		
West	550	550		

Using the equation below :

$$\Delta t_e = 0.55 [\sigma_s/\sigma_m]. \Delta t_{em} + [1 - 0.55([\sigma_s/\sigma_m]). \Delta t_{es}$$

The table is updated to :

[illegible]

### Thermal Resistances of the walls

Conduction thru the North Wall							
Material				t	A	k or C	R
Face Brick				0.1025	100	0.82	0.00125
Plastered Brick				0.1025	100	0.82	0.00125
Air gap				0.05	100	6.2	0.00161
Plastered Brick				0.02	100	0.38	0.00053
UA							215.554

Conduction thru the East and West Wall							
Material				t	A	k or C	R
Face Brick				0.1025	50	0.82	0.0025
Plastered Brick				0.1025	50	0.82	0.0025
Air gap				0.05	50	6.2	0.0032258
Plastered Brick				0.02	50	0.38	0.00105
UA							107.67676

### Final Heat Heat Gain through the walls

Now using  $Q = U.A. \Delta t_e$ , the final heat load results in :

[illegible]

## Heat Gain through the roof

### Roof Construction

200 mm thk. CONCRETE
50 mm Think Pink Insulation
20 mm thk. plaster board (insulation)

Mass/area of the roof

$$\begin{aligned} \text{Mass/area (concrete)} &= \text{density(dense concrete) x thickness} \\ &= 2320 \times 0.2 = \underline{464 \text{ kg/m}^2} \end{aligned}$$

$$\begin{aligned} \text{Mass/area (plasterboard)} &= \text{density x thickness} \\ &= 950 \times 0.02 = \underline{19 \text{ kg/m}^2} \end{aligned}$$

$$\begin{aligned} \text{Mass/area(insulation)} &= \text{density x thickness} \\ &= 500 \times 0.05 = \underline{25 \text{ kg/m}^2} \end{aligned}$$

$$\text{Total mass/area of the roof} = \underline{508 \text{ kg/m}^2}$$

EQUIVALENT TEMPERATURE DIFFERENCE												Mass/area
	AM					PM						
Sun Time	8	9	10	11	12	1	2	3	4	5	6	
delta_t_em	8.3	8.3	8.9	9.4	11.1	14.4	16.7	17.8	20	21.7	22.8	400kg/m^2
delta_t_es	1.1	1.1	1.1	1.7	2.2	3.3	4.4	5.6	6.7	7.2	7.8	300kg/m^2
The tables provided dosent mass/area for 508 kg/m^2, so the cloasest values were used...												

### Correction for indoor/outdoor temp. difference and the daily range

Outdoor temperature (Cape town at 3pm) - Room design temperature =  $32.2 - 24 = \underline{8.2^\circ\text{C}}$ .

January daily range =  $32.2 - 22.2 = 10^\circ\text{C}$ , the correction factor as  $\underline{-1.8^\circ\text{C}}$ .

The corrected table is below :

	AM					PM						
Sun Time	8	9	10	11	12	1	2	3	4	5	6	
delta_t_em	6.5	6.5	7.1	7.6	9.3	12.6	14.9	16	18.2	19.9	21	
delta_t_es	-0.7	-0.7	-0.7	-0.1	0.4	1.5	2.6	3.8	4.9	5.4	6	

### Correction for Month and Latitude

EQUIVALENT TEMPERATURE DIFFERENCE											
	AM					PM					
Sun Time	8	9	10	11	12	1	2	3	4	5	6
delta_t_e	6.7	6.7	7.3	7.8	9.6	12.9	15.3	16.4	18.6	20.3	21.5

Cape Town – Latitude – 33°55'; Longitude – 18°27' - Reference attached

EQUIVALENT TEMPERATURE DIFFERENCE											
	AM					PM					
Sun Time	8	9	10	11	12	1	2	3	4	5	6
delta_t_em	6.5	6.5	7.1	7.6	9.3	12.6	14.9	16	18.2	19.9	21
delta_t_es	-0.7	-0.7	-0.7	-0.1	0.4	1.5	2.6	3.8	4.9	5.4	6

From Table 5 - Peak Solar Heat Gains:

$$\sigma_m = 790 \text{ W/m}^2 \text{ (40° South latitude).}$$

$$\sigma_s = 814 \text{ W/m}^2 \text{ by interpolation (33,9166° ~ 34°).}$$

Using the equation below :

$$\Delta t_e = [\sigma_s / \sigma_m] \cdot [\Delta t_{em} - \Delta t_{em}]$$

The corrected values are below

EQUIVALENT TEMPERATURE DIFFERENCE											
	AM					PM					
Sun Time	8	9	10	11	12	1	2	3	4	5	6
delta_t_e	6.7	6.7	7.3	7.8	9.6	12.9	15.3	16.4	18.6	20.3	21.5

### Conduction through the roof

$$Q = U \times A \times \Delta t_e$$

Conduction through the roof							
Material				t	A	k	R
Concerete				0.2	800	1.5	0.00017
Plasterboard				0.02	800	0.16	0.00016
Insulation(think pink)				0.05	800	0.045	0.00139
UA							584

Below is the heat gain through the roof

THROUGH THE ROOF (Watts)												
	AM					PM						
Sun Time	8	9	10	11	12	13	14	15	16	17	18	
Heat gain	3924.9	3924.9	4286.1	4576.4	5590.8	7557.6	8922.6	9563.4	10868.1	11882.5	12534.0	

### Heat gain through the windows via conduction/convection

$$U = [1/\alpha_{\text{outside}} + t_{\text{glass}}/k + 1/\alpha_{\text{inside}}]$$

For January, the heat transfer coefficient,  $\alpha_{\text{outside}} = 30 \text{ W/m}^2\cdot\text{K}$  (ASSUMED)  
 For June, the heat transfer coefficient,  $\alpha_{\text{outside}} = 29 \text{ W/m}^2\cdot\text{K}$  (ASHRAE :30.5)  
 Heat transfer coefficient inside (all year)  $= 8.3 \text{ W/m}^2\cdot\text{K}$  (ASHRAE :30.6)

Heat Transfer through glass								
			JAN				JUN	
ho			30				29	
hi			8.3				8.3	
glass			1.05				1.05	
U			6.382745				6.3362591	

### Inside and outside temperature difference

Outside temp.(table-pg 31) - indoor temp(24 deg. C).											
Sun Time	8	9	10	11	12	13	14	15	16	17	18
$\Delta t_e$	1.6	2.7	3.2	4.3	5.4	6.6	7.7	8.2	7.7	7.1	7.2

Heat Load,  $Q = U.A. \Delta t_e$

HEAT GAIN (Watts) $Q = U.A.\Delta t_e$ (conduction/convection)											
Sun Time	8	9	10	11	12	13	14	15	16	17	18
Exposure											
North	408.5	689.3	817.0	1097.8	1378.7	1685.0	1965.9	2093.5	1965.9	1812.7	1838.2
East	204.2	344.7	408.5	548.9	689.3	842.5	982.9	1046.8	982.9	906.3	919.1
West	204.2	344.7	408.5	548.9	689.3	842.5	982.9	1046.8	982.9	906.3	919.1



## Solar Heat gain through windows

Mass per unit area of buildings

Mass/area of the building						
		No.	kg/m <sup>2</sup>	m <sup>2</sup>		mass
North/South Walls		2	400	100		80000
East/West		2	400	50		40000
Roof			508	800		406400
Total mass						526400
Mass/area						658 kg/m <sup>2</sup>

Use 700 kg/m<sup>2</sup> from table 7. The difference in using 658 or 700 is not significant.

Month	January						
North Exposure							
24 hr operation of airconditioner							
							Q_actual
Time	Area		SHGF max	SF	SASH	CLF	
8	40		152	0.15	1.1765	0.13	139.48
9	40		152	0.15	1.1765	0.2	214.59
10	40		152	0.15	1.1765	0.28	300.42
11	40		152	0.15	1.1765	0.35	375.53
12	40		152	0.15	1.1765	0.43	461.36
13	40		152	0.15	1.1765	0.49	525.74
14	40		152	0.15	1.1765	0.52	557.93
15	40		152	0.15	1.1765	0.52	557.93
16	40		152	0.15	1.1765	0.49	525.74
17	40		152	0.15	1.1765	0.42	450.64
18	40		152	0.15	1.1765	0.37	396.99

Month	January						
East Exposure							
24 hr operation of airconditioner							
							Q_actual
Time	Area		SHGF max	SF	SASH	CLF	
8	20		550	0.15	1.1765	0.34	660.00
9	20		550	0.15	1.1765	0.4	776.47
10	20		550	0.15	1.1765	0.41	795.88
11	20		550	0.15	1.1765	0.39	757.06
12	20		550	0.15	1.1765	0.34	660.00
13	20		550	0.15	1.1765	0.3	582.35
14	20		550	0.15	1.1765	0.28	543.53
15	20		550	0.15	1.1765	0.26	504.71
16	20		550	0.15	1.1765	0.23	446.47
17	20		550	0.15	1.1765	0.22	427.06
18	20		550	0.15	1.1765	0.2	388.24

Month	January						
West Exposure							
24 hr operation of airconditioner							
							Q_actual
Time	Area		SHGF max	SF	SASH	CLF	
8	20		550	0.15	1.1765	0.11	213.53
9	20		550	0.15	1.1765	0.1	194.12
10	20		550	0.15	1.1765	0.1	194.12
11	20		550	0.15	1.1765	0.1	194.12
12	20		550	0.15	1.1765	0.1	194.12
13	20		550	0.15	1.1765	0.13	252.35
14	20		550	0.15	1.1765	0.19	368.82
15	20		550	0.15	1.1765	0.27	524.12
16	20		550	0.15	1.1765	0.36	698.82
17	20		550	0.15	1.1765	0.43	834.71
18	20		550	0.15	1.1765	0.45	873.53

Total solar heat gain through windows

SOLAR HEAT TOTALS											
Sun Time	8	9	10	11	12	13	14	15	16	17	18
HEAT	1013.0	1185.2	1290.4	1326.7	1315.5	1360.4	1470.3	1586.8	1671.0	1712.4	1658.8

### **Heat Gain – Individual Walls - Total**

**(Walls +Window(Solar Heat Gain)+Window(convection/conduction))**

HEAT GAIN TOTALS (Watts) - INDIVIDUAL WALLS											
Sun Time	8	9	10	11	12	13	14	15	16	17	18
Exposure											
North	440.2	860.8	1128.2	1744.7	2274.9	3065.9	3706.2	4036.6	4029.6	3853.3	3799.7
East	954.8	1605.6	1947.0	2175.7	2299.4	2249.9	2307.0	2287.3	2156.6	2069.5	2043.2
West	508.3	643.9	719.8	907.4	1092.5	1424.9	1803.4	2244.5	2542.4	2841.7	3053.1

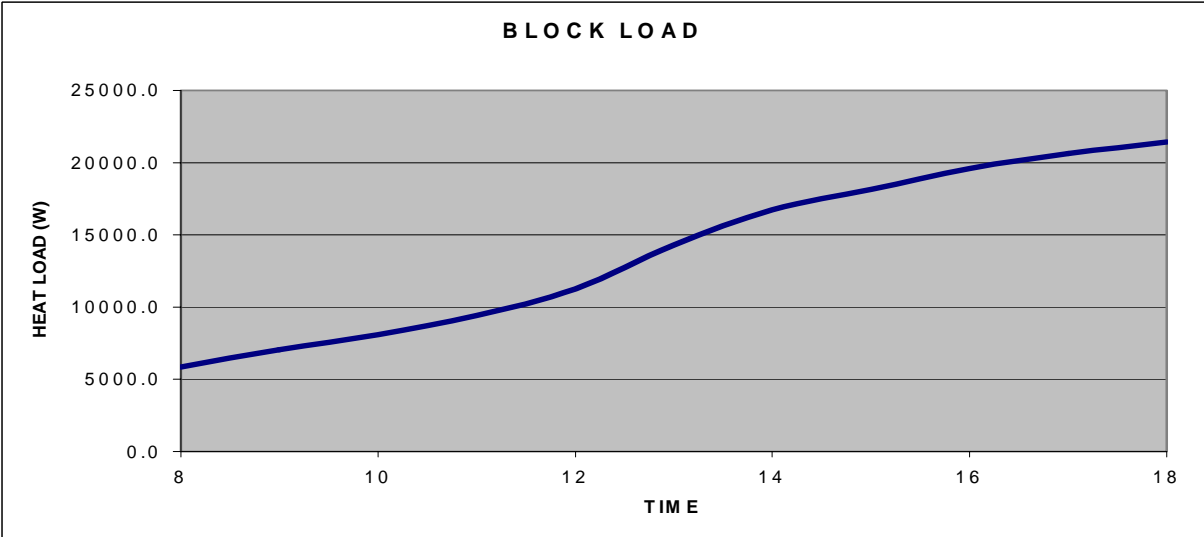
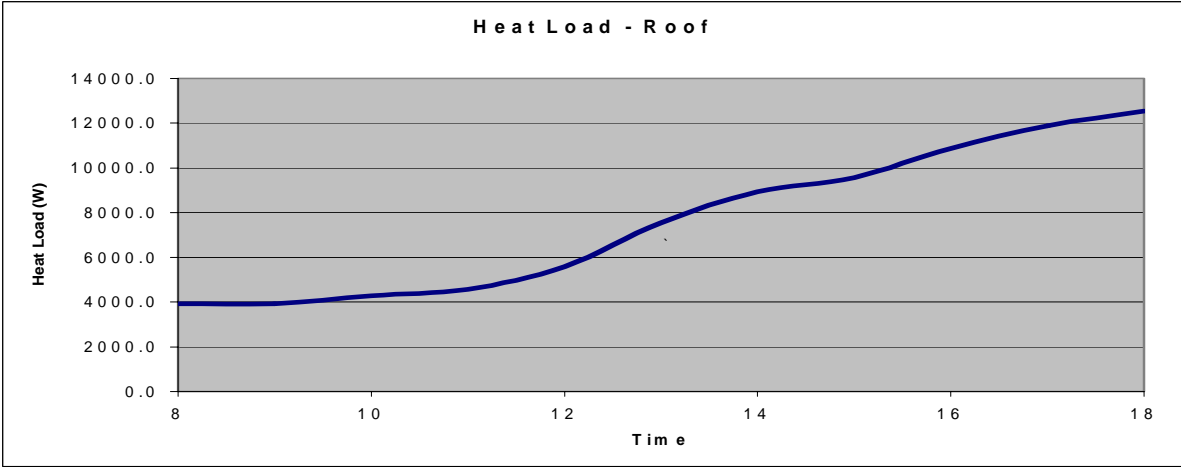
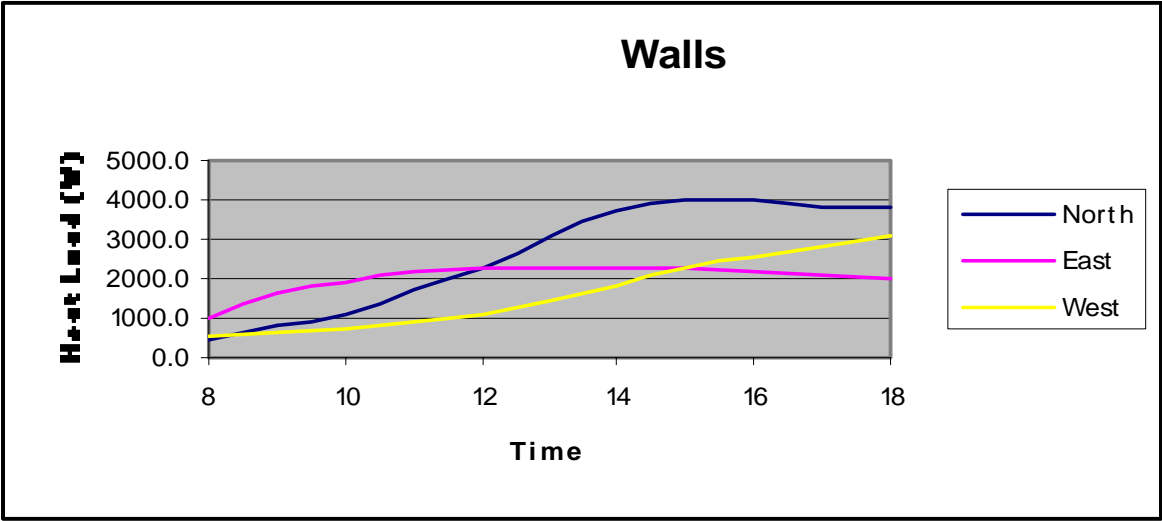
### **Block Load**

Below is the block load,

Heat gain through walls + Heat gain Through Windows + Heat gain through Roof

BLOCK LOAD - WALLS + WINDOWS + ROOF											
Sun Time	8	9	10	11	12	13	14	15	16	17	18
BLOCK LOAD	5828.2	7035.2	8081.0	9404.2	11257.7	14298.4	16739.1	18131.8	19596.7	20647.0	21430.0

**PLOTS FOR JANUARY**



PLOTS FOR JUNE (same procedure was followed as for January)

